

# Flory–Huggins interaction parameter of poly(ethylene oxide)/poly(epichlorohydrin) and poly(ethylene oxide)/poly(epichlorohydrin-co-ethylene oxide) blends

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Blends of poly(ethylene oxide) with poly(epichlorohydrin) and poly(epichlorohydrin-co-ethylene oxide) have been prepared by the freeze-drying method from benzene solutions of the polymer mixture at different compositions. The miscibility of the mixtures was studied by DSC. A single glass transition temperature is observed for all the blends studied. Measurement of the melting temperature ( $T_m$ ) depression for the blends allowed determination of the Flory–Huggins interaction parameter ( $\chi_{12}$ ) of the two polymers in the melt using the Nishi–Wang equation. The Hoffman–Weeks extrapolation was applied to obtain equilibrium  $T_m$  data. The values of the  $\chi_{12}$  obtained from  $T_m$  depression data were negative for all blends. This suggests the miscibility of the components of the blends. © 1998 Published by Elsevier Science Ltd. All rights reserved.

(Keywords: poly(ethylene oxide); poly(epichlorohydrin); poly(epichlorohydrin-co-ethylene oxide))

## INTRODUCTION

There have been many studies of polymer blends in recent years. The interest in novel structures and properties of blends still motivates extensive studies, as does the increasing importance in practical applications of new polymeric materials having a wide range of physical and/or physicochemical properties, without similar behavior in homopolymers<sup>1</sup>. Recently, interest has been attracted to systems in which at least one of the components is crystallizable. In this case, a melt point depression of the crystalline phase relative to its melting point ( $T_m$ ) in a non-interacting medium provides additional evidence of miscibility<sup>2</sup>. The crystalline polymer poly(ethylene oxide), PEO, has a  $T_m$  at ca 65°C and glass transition in the temperature range from –53 to –45°C. Above the melting point it can be processed as a thermoplastic<sup>1,3</sup>. Blends of PEO with poly(methyl methacrylate), PMMA<sup>4–7</sup>, poly(vinyl acetate), PVAc<sup>8–10</sup>, poly(3-hydroxybutyrate), PHB<sup>11</sup>, and others, have been studied with emphasis on phase behavior. In these blends, miscibility, crystallization kinetics, morphology and the phase behavior were studied<sup>10,12–14</sup>. Poly(epichlorohydrin), PECH, is a linear and amorphous elastomer, exhibiting a glass transition temperature at –23°C. Epichlorohydrin copolymer rubber, P(ECH-co-EO), with equimolar amounts of epichlorohydrin, ECH, and ethylene oxide, EO, has been used in various branches of technology, such as in the automotive industry, in fuel, lubricating fluids, air and vacuum hoses and others<sup>15</sup>. There are few published papers on PECH and the majority of publications were about properties, characterization and chemical modification<sup>16–18</sup>. PECH has been studied in blends with PHB<sup>19</sup>, polyacrylates<sup>20</sup> and aliphatic polyesters<sup>21</sup>.

In this work, we investigate the miscibility of blends of PEO with PECH and with P(ECH-co-EO) using differential scanning calorimetry (DSC). The Flory–Huggins interaction parameter was determined by the PEO melting point depression method.

## EXPERIMENTAL

### Materials

The polymers used in this work are listed in *Table 1*.

The molar mass ( $M_n$ ) were determined by gel permeation chromatography (GPC) on a Waters chromatograph (model II A) using three linear columns (Ultrastaygel molecular weight range from  $2.0 \times 10^3$  to  $4.0 \times 10^6$  g mol<sup>-1</sup>) with a Waters differential refractometer (model 410) as detector.

### Blends preparation

The blends were prepared by the freeze-drying method from benzene solutions of polymer mixtures at 5 wt% concentration. Blends with different compositions were prepared: 20, 40, 60, 80 wt% in PEO. The mixtures were dried under vacuum until constant weight and then stored in a desiccator. Films of the blends were obtained by pressing at 130°C for 5 min at 25 MPa and 10 min at 50 MPa.

### Characterization of blends by DSC

The DSC curves for the homopolymers and the blends were obtained on a T.A. Instruments model 2100 coupled to a T.A. 2100 data analysis system. Sample weights were maintained in the range of 18–20 mg. All experiments were performed under nitrogen flow of 100 mL min<sup>-1</sup>. The samples were first held at 100°C for 5 min to eliminate the thermal history. After cooling the samples to –100°C at a rate of 10°C min<sup>-1</sup>, they were heated again to 100°C at a rate of 10°C min<sup>-1</sup>. The DSC curves shown in this work and used to construct the phase diagrams correspond to the

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**Table 1** Polymers used in this study

Polymer	Code	Source	$M_n$ (g mol <sup>-1</sup> )	$M_w/M_n$
poly(ethylene oxide)	PEO	Aldrich	$1.0 \times 10^5$	2
poly(epichlorohydrin)	PECH	Aldrich	$1.6 \times 10^5$	4
poly(epichlorohydrin-co-ethylene oxide)	P(ECH-co-EO)	Zeon Chemicals	$2.8 \times 10^5$	4

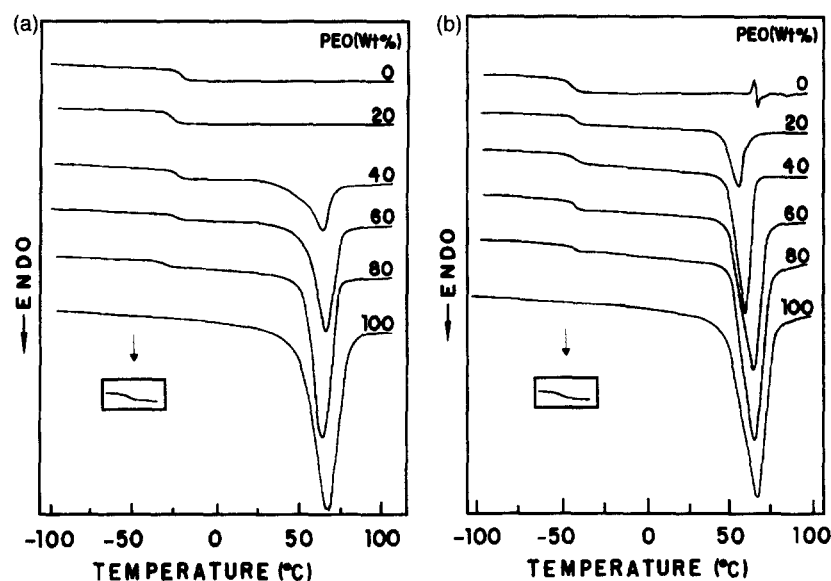
heating scan. All DSC curves were normalised with respect to mass. The glass transition temperature and the melting temperature were assumed as the half height of the step and the maximum of the peak, respectively. Enthalpy of melting was obtained by integration of the peak area.

#### Determination of the equilibrium melting temperature

The isothermal crystallization was performed on the DSC equipment based on the Hoffman–Weeks method<sup>22</sup>. The weight of the PEO and the blends was maintained in the region of 12 mg. The isothermal crystallization experiment was carried out using the following procedure: the samples were heated to 100°C, kept at this temperature for 5 min, rapidly cooled (cooling rate  $> 40^\circ\text{C min}^{-1}$ ) to the desired crystallization temperature ( $T_c$ ) and maintained at this temperature for 20 min. After the isothermal crystallization was completed, the samples were cooled to 20°C and heated to 100°C at a rate of  $10^\circ\text{C min}^{-1}$  for the measurement of the  $T_m$ . This procedure was repeated for different crystallization temperatures.

## RESULTS AND DISCUSSION

Figure 1a shows DSC curves of PEO and its blends with PECH and Figure 1b with P(ECH-co-EO). PECH and P(ECH-co-EO) exhibit glass transition ( $T_g$ ) at  $-23^\circ\text{C}$  and  $-42^\circ\text{C}$ , respectively. PEO exhibits  $T_g$  at  $-50^\circ\text{C}$  and  $T_m$  at  $68^\circ\text{C}$  (Table 2). For P(ECH-co-EO) we also observed a reproducible crystallization peak followed by melting. In this case the crystalline phase is probably formed by organization of the ethylene oxide blocks present in the copolymer structure. A single  $T_g$  is observed for all blends studied. It does not change appreciably with the composition, showing values near to the  $T_g$  of the pure PECH or P(ECH-co-EO), suggesting that the amorphous phase is rich in elastomer. The blends show also a single endothermic peak corresponding to the melting of the PEO phase (Table 2). The  $T_m$  of PEO is depressed by the presence of the second component, PECH or P(ECH-co-EO), indicating a favourable polymer–polymer interaction, Figure 2. Blends of PEO/PECH only exhibit crystallinity above 20 wt% of PEO, while blends with P(ECH-co-EO) exhibit crystallinity


**Figure 1** DSC curves for blends: (a) PEO/PECH and (b) PEO/P(ECH-co-EO). Heating rate =  $10^\circ\text{C min}^{-1}$ 
**Table 2** Glass transition temperature ( $T_g$ ), melting point ( $T_m$ ) and degree of crystallinity ( $X_c$ ) of PEO/PECH and PEO/P(ECH-co-EO) blends

PEO (wt%)	PECH			P(ECH-co-EO)		
	$T_g$ (°C)	$T_m$ (°C)	$X_c$ (%)	$T_g$ (°C)	$T_m$ (°C)	$X_c$ (%)
0	$-23 \pm 3$	-	-	$-42 \pm 3$	$65 \pm 1$	-
20	$-27 \pm 3$	-	-	$-42 \pm 3$	$56 \pm 1$	$15 \pm 3$
40	$-27 \pm 3$	$63 \pm 1$	$18 \pm 3$	$-42 \pm 3$	$59 \pm 1$	$24 \pm 3$
60	$-26 \pm 3$	$65 \pm 1$	$33 \pm 2$	$-43 \pm 4$	$65 \pm 1$	$47 \pm 2$
80	$-32 \pm 3$	$63 \pm 1$	$51 \pm 1$	$-44 \pm 5$	$65 \pm 1$	$60 \pm 1$
100	$-50 \pm 5$	$68 \pm 1$	$73 \pm 1$	$-50 \pm 5$	$68 \pm 1$	$73 \pm 1$

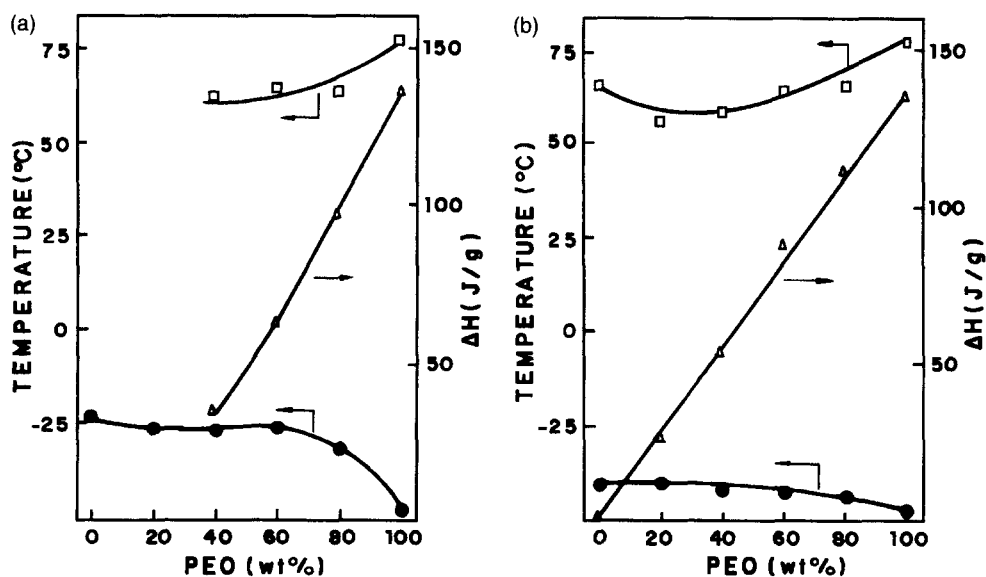


Figure 2 Phase diagrams for blends: (a) PEO/PECH and (b) PEO/P(ECH-co-EO). (□) melting point; (Δ) enthalpy of fusion; (●) glass transition temperature

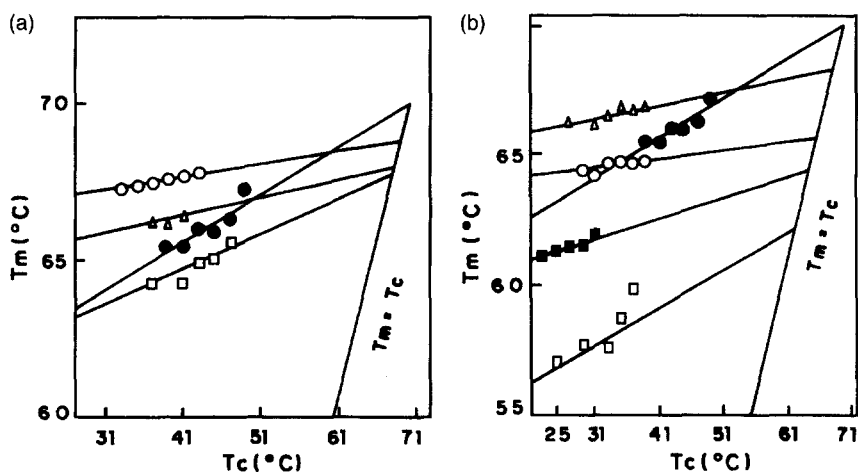


Figure 3 Hoffman–Weeks plots for isothermally crystallised blends: (a) PEO/PECH and (b) PEO/P(ECH-co-EO) blends. PEO (wt%): (●) 100; (Δ) 80; (○) 60; (□) 40; and (■) 20

for all studied compositions. The degree of crystallinity ( $X_c$ ) of the PEO phase and of the blends are calculated using equation (1), where  $\Delta H_f$  is the enthalpy of melting per gram of 100% crystalline PEO ( $188 \text{ J g}^{-1}$ )<sup>13</sup> and  $\Delta H_f^*$  is the apparent enthalpy of melting per gram of blend.

$$X_c = \Delta H_f^* / \Delta H_f \quad (1)$$

The degree of crystallinity ( $X_c$ ) of the blends decreases for all compositions with increase in concentration of PECH and P(ECH-co-EO). This effect is more pronounced for blends of PEO/PECH (Table 2) and it is not expected, because the molar mass of the copolymer is higher than the homopolymer (see Table 1), resulting probably in higher viscosity in the melt for the first system. The melting viscosity affects the crystallization kinetics and, for the same crystallization conditions, blends with P(ECH-co-EO) should achieve lower crystallization degrees in comparison to blends of PECH, in absence of other factors. However, the crystallization is favourable for blends of P(ECH-co-EO) suggesting that crystallizable ethylene oxide blocks in the copolymer act as crystallization nuclei depressing the activation barrier to the nucleation process. This results in an increase of the overall crystallization rate.

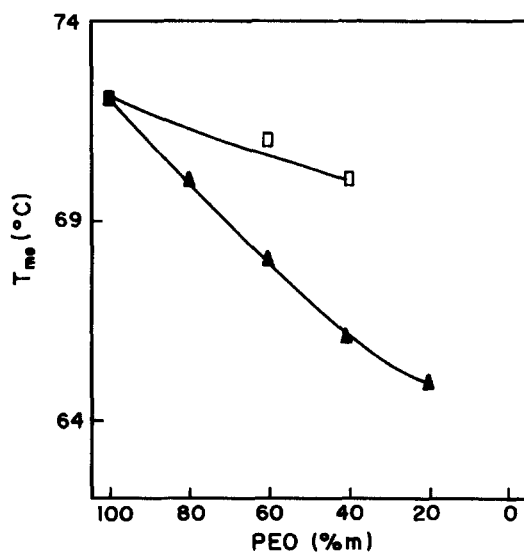


Figure 4  $T_m$  as a function of blend composition: (□) PEO/PECH blends and (▲) PEO/P(ECH-co-EO) blends

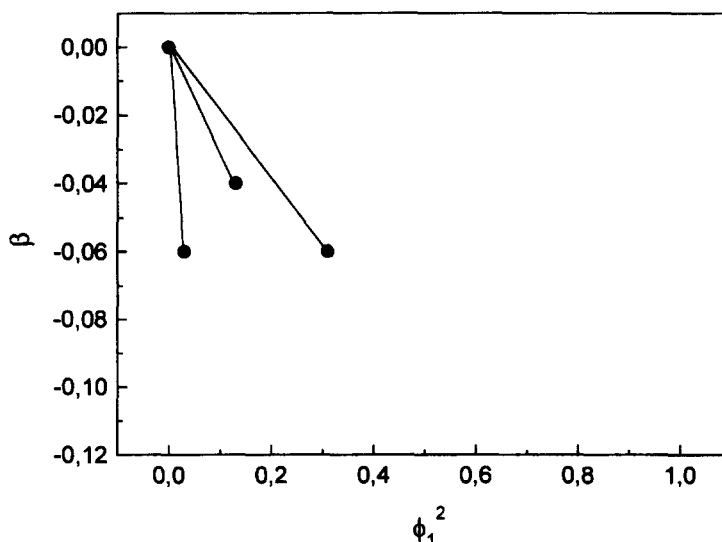
Polymer–polymer interaction parameter

The DSC study has already revealed that the  $T_m$  of PEO is depressed systematically with the increase of PECH and P(ECH-co-EO) content in the binary blends. This phenomenon may be explained in terms of thermodynamic mixing, by the exothermic interaction between a crystalline and an amorphous polymer and in terms of kinetic or morphological factors. The kinetic effects result because crystals are formed at temperatures below the equilibrium melting and this can be avoided using equilibrium melting temperatures. Morphological effects are associated with changes in crystal perfection or geometry and with different thermal histories of the samples<sup>23</sup>. The contribution of such morphological effects can usually be removed by constructing a Hoffman–Weeks plot<sup>22</sup> using melting data for PEO and for blends isothermally crystallized at different temperatures ( $T_c$ ). The equilibrium melting temperature ( $T_{me}$ ) is determined

by the extrapolation of the experimental curve of  $T_m$  versus  $T_c$  to the theoretical curve corresponding to  $T_m = T_c$  (Figure 3) assuming that the crystals are perfect and of finite size and that no recrystallization takes place during the melting run.

A value of  $T_{me}$  of 70°C was obtained for pure PEO and melting point depressions were observed in blends with PECH and [P(ECH-co-EO)] (Figure 4). The copolymer is more efficient in depressing the melting point of the crystalline phase of PEO in comparison to the homopolymer. The melting point depression can be due to the decrease of the chemical potential of the crystallizable polymer caused by the addition of the miscible diluent. The expression to describe the dependence of the melting point depression due only to thermodynamic effects on the blends composition is given, according to the Flory–Huggins theory modified by Nishi–Wang<sup>11,13,23,24</sup> in equation (2).

a)



b)

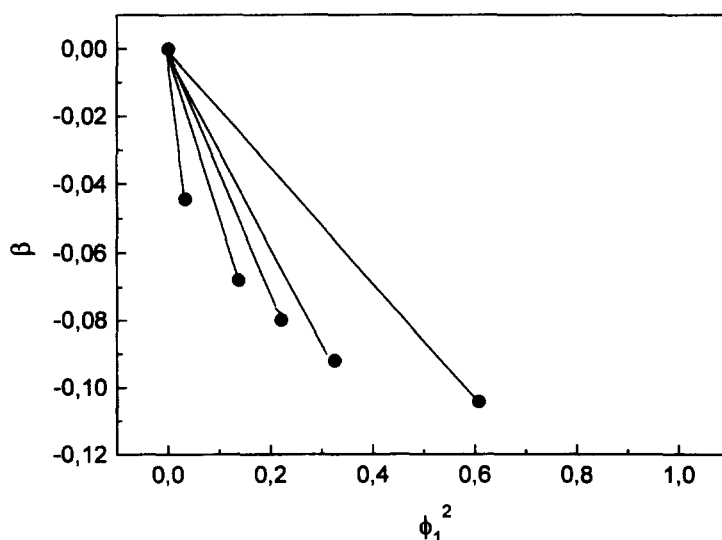


Figure 5 Plots of  $\beta$  versus  $\phi_1^2$  according to equation (3) for blends: (a) PEO/PECH and (b) PEO/P(ECH-co-EO)

**Table 3** Polymer–polymer interaction parameter ( $\chi_{12}$ ) for PEO/PECH blends and PEO/P(ECH-co-EO) blends

PEO (wt%)	PEO/PECH	PEO/P(ECH-co-EO)
20	-	$-0.17 \pm 0.03$
40	$-0.19 \pm 0.03$	$-0.28 \pm 0.04$
60	$-0.21 \pm 0.01$	$-0.50 \pm 0.02$
80	$-0.91 \pm 0.02$	$-1.35 \pm 0.02$

$$\begin{aligned} (1/T_{me} - 1/T_{me}^0) = & - (RV_{2u}/\Delta H_{2u}V_{1u})[\ln\phi_2/m_2 \\ & + (1/m_2 - 1/m_1)\phi_1 + \chi_{12}\phi_1^2] \end{aligned} \quad (2)$$

In equation (2),  $T_{me}$  and  $T_{me}^0$  are the equilibrium melting points of the blends and pure PEO, respectively. Subscript 1 identifies the polymer additive (P(ECH-co-EO) and PECH) and subscript 2 the crystallizable polymer (PEO).  $V_u$  is the molar volume of the repeating unit,  $\Delta H_{2u}$  is the enthalpy of fusion per mole of repeating unit,  $m$  is the degree of polymerization,  $\phi$  are the volume fractions,  $R$  is the universal gas constant and  $\chi_{12}$  is the polymer–polymer interaction parameter. By rearranging the terms of equation (2) we obtain equation (3).

$$\begin{aligned} - [(\Delta H_{2u}V_{1u}/RV_{2u})(1/T_{me} - 1/T_{me}^0)] \\ - \ln\phi_2/m_2 - (1/m_2 - 1/m_1)\phi_1 = \beta = \chi_{12}\phi_1^2 \end{aligned} \quad (3)$$

A plot of  $\beta$  versus  $\phi_1^2$  should give a straight line passing through the origin if  $\chi_{12}$  is assumed to be independent of the composition. The plots shown in *Figure 5* were obtained using the following parameters:  $\Delta H_{2u} = 8.26 \text{ KJ mol}^{-1}$ ;  $R = 8.31 \text{ J K}^{-1} \text{ mol}^{-1}$ ;  $V_{PECH} = 67.6 \text{ cm}^3 \text{ mol}^{-1}$ ;  $V_{PEO} = 38.9 \text{ cm}^3 \text{ mol}^{-1}$ ;  $V_{[P(ECH-co-EO)]} = 53.7 \text{ cm}^3 \text{ mol}^{-1}$ ;  $m_{PECH} = 1081$ ;  $m_{PEO} = 2273$ ;  $m_{[P(ECH-co-EO)]} = 4102$ . For PEO/PECH blends the points are dispersed and for PEO/P(ECH-co-EO) blends  $\beta$  presents a logarithmic dependence on  $\phi_1^2$ , suggesting a composition dependence of  $\chi_{12}$ . In this case the interaction parameter, at different blend compositions (*Table 3*), can be obtained as the slope of the lines connecting each experimental point and the origin, as shown in *Figure 5*. The values of  $\chi_{12}$  calculated according to this method are negative for all investigated compositions indicating miscibility of PEO with PECH and with P(ECH-co-EO) in the melt.

Min *et al.*<sup>25</sup> also studied blends of PEO and PECH and found that the  $\chi_{12}$  parameter is not dependent on the composition ( $\chi_{12} = -1.04$ ). But, in this case, materials with different molar mass and polydispersity were used and the blends were prepared by casting. These factors can be responsible for the observed behavior. The values of  $\chi_{12}$  obtained for PEO/PECH and PEO/P(ECH-co-EO) blends were comparable to those described in the literature for other blends, as shown in *Table 4*.

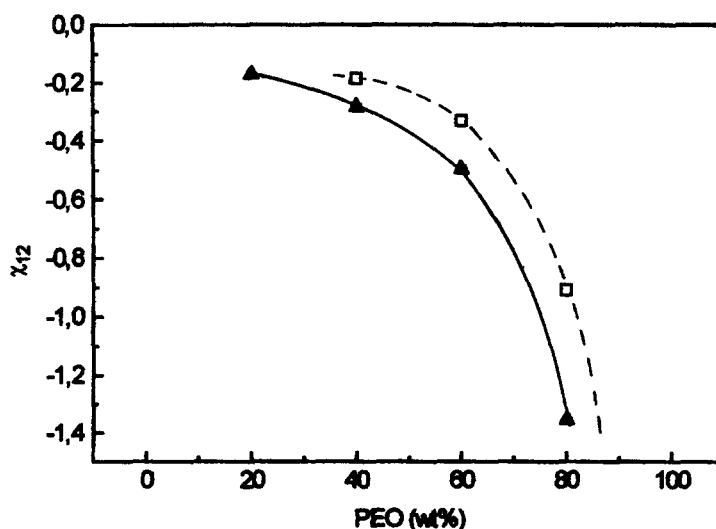
Nishi and Wang attribute the dependence of  $\chi_{12}$  on the blend composition to morphological and kinetics factors,

**Table 4** Values of  $\chi_{12}$  for blends described in the literature

Blends	$\chi_{12}$	Reference
PEO( $M_w = 4.0 \times 10^6 \text{ g mol}^{-1}$ )/PMMA( $M_w = 4.0 \times 10^6 \text{ g mol}^{-1}$ )	-0.131	2
PEO( $M_w = 3.65 \times 10^6 \text{ g mol}^{-1}$ )/PMMA( $M_w = 9.36 \times 10^4 \text{ g mol}^{-1}$ )	-0.139	2
PEO( $M_w = 2.0 \times 10^4 \text{ g mol}^{-1}$ )/aPMMA( $M_w = 1.31 \times 10^5 \text{ g mol}^{-1}$ )	-0.29	13
PEO( $M_w = 3.0 \times 10^5 \text{ g mol}^{-1}$ )/PVAc( $M_w = 1.6 \times 10^5 \text{ g mol}^{-1}$ )	-0.30	14
PEO( $M_w = 2.0 \times 10^3 \text{ g mol}^{-1}$ )/PHB( $M_w = 2.79 \times 10^3 \text{ g mol}^{-1}$ )	<sup>a</sup>	11
PECH( $M_w = 2.0 \times 10^4 \text{ g mol}^{-1}$ )/PEMA( $M_w = 1.5 \times 10^5 \text{ g mol}^{-1}$ )	-1.08	23
PECH( $M_w = 7.0 \times 10^5 \text{ g mol}^{-1}$ )/PHB( $M_w = 1.5 \times 10^4 \text{ g mol}^{-1}$ )	<sup>b</sup>	19
PECH( $M_w = 5.55 \times 10^5 \text{ g mol}^{-1}$ )/PEO( $M_w = 3.0 \times 10^5 \text{ g mol}^{-1}$ )	-1.04	25
PECH( $M_w = 7.0 \times 10^5 \text{ g mol}^{-1}$ )/PEO( $M_w = 5.0 \times 10^4 \text{ g mol}^{-1}$ )	-0.172	26

<sup>a</sup> depends on the blend composition, varying from -0.21 to -2.0

<sup>b</sup> depends on the blend composition varying from -0.054 to -0.058


**Figure 6**  $\chi_{12}$  as a function of blend composition: ( $\square$ ) PEO/PECH blends and ( $\blacktriangle$ ) PEO/P(ECH-co-EO) blends. Dashed line represents  $\chi_{12}$  as a function of the total ethylene oxide content in the PEO/P(ECH-co-EO) blends

such as recrystallization, phase segregation, etc.<sup>11,14,19,27</sup>. However, Painter *et al.*<sup>28</sup> proposed that this effect results from the strong interactions between the different components, such as hydrogen bonding observed in poly(vinyl phenol) and poly(ethylene-co-acrylic acid) blends. In the present work, the interaction between the blend components are mainly of the dipole–dipole type, which can also be responsible for the strong dependence of  $\chi_{12}$  on the composition. It is very interesting to observe that  $\chi_{12}$  decreases for rich PEO blends, and that, despite the higher molar mass of P(ECH-co-EO), its blends present lower  $\chi_{12}$  values in comparison to blends of PECH, as can be observed in Table 3. The meaning of the first observation is a decrease of the interaction energy density or miscibility as the elastomer concentration increases. The second observation implies that the interaction energy density is higher for PEO/P(ECH-co-EO) in comparison with PEO/PECH. If we consider that only interaction between epichlorohydrin segments in both homopolymer and copolymer and ethylene oxide segments in PEO contribute effectively to the blend miscibility, the lower value for  $\chi_{12}$  for blends containing copolymer can be understood as a simple dilution effect. Blends with the copolymer have lower epichlorohydrin concentration in comparison to the blends of the homopolymer at the same composition. In Figure 6 we show the dependence of  $\chi_{12}$  on the blend composition. The dashed line represents  $\chi_{12}$  values for PEO/P(ECH-co-EO) blends as a function of the total ethylene oxide segments in the blend and it fits the experimental data for PEO/PECH blends.

## CONCLUSIONS

Binary blends of PEO with PECH and P(ECH-co-EO) obtained by the freeze-drying method are miscible, as demonstrated by the presence of only one glass transition temperature for all the compositions investigated and by the systematic depression of the melting temperature of PEO with an increase in PECH and P(ECH-co-EO) content. The observation of the thermal transitions enable us to reasonably conclude that the polymer pairs are thermodynamically miscible. The polymer–polymer interaction parameters obtained from thermodynamic melting temperature depression analysis are negative and exhibit dependence on the blend composition, decreasing for blends rich in PEO. PEO/P(ECH-co-EO) blends are more miscible than the corresponding PEO/PECH blends and this is attributed to the lower epichlorohydrin concentration in the blends of the copolymer.

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